Explosion of Resin Factory in Osaka [August 20th, 1982 Sakai, Osaka, Japan]

Haruhiko Itagaki. (National Institute of Industrial Safety) Mitsuo Kobayashi (Graduate School of Frontier Science, University of Tokyo) Masamitsu Tamura (Graduate School of Frontier Sciences, University of Tokyo)

This accident is an interesting example for considering the safety of a chemical plant and the ways of establishing effective countermeasures after the occurrence of an accident.

At midnight on August 20th, 1982, there was a relatively small explosion at a resin manufacturing p lant of Daicel Chemical I ndustries, Co., Ltd . at the Sakai manufacturing complex in Sakai, Osaka, and the order to stop the plant was issued. During the shutdown procedure of the plant, gas leaked from a monomer mixing drum that contained two kinds of monomers as raw materials and a catalyst. The occurrence of the leak was informed to the meeting of the managing staff who were discussing the countermeasures to be taken to the first explosion. When all of the members attending the meeting rushed to the leakage site, the second large explosion suddenly occurred. This second explosion resulted in six fatalities, nine seriously injured, and 198 sligh tly injured persons. 178 of the 198 persons who we re slightly injured were inhabitants of the nearby area. Furthermore, the number of houses damaged in the accident was over 1700.

Before the first exp losion, agitation of the polym erization re actor and supply o f lukewarm water to the cooling jacket had st opped due to a po wer failure. In order to keep the reactor c ool, cold co oling water was used inste ad of the lukewarm w ater immediately. Howev er, the reaction led to a runaway reaction, and monomers evaporated. The evap orated gas by passed the combustion deodorization furnace that had been designed on the assump tion of usual exhaust gas proces sing, and the explosion occurred at the inlet of the stack. However, this first exp losion did not cause any human damage or large physical damage.

The shutdown procedure of the plant was executed in the settlement of the accident, and at the same ti me, the managing staff held a meeting to discuss the countermeasures to b e taken. The next day, the shutdo wn pro cedure and t he countermeasure meeting were continued. In the evening, a gas leakage occurred from a monomer mixing drum, which contained the monomers with which the reactor will be charged. The gas leakage gradually increased, and no body could get near the leakage place. On hearing the news, all of the members who were attending the meeting came to the leakage site. At that moment, a large explosion occurred. All human damage and large physical damage occurred in this second explosion.

While a liquid mixture of acryloni trile, st yrene and a p olymerization catalyst of organic peroxide was left in the monomer mixing drum for 42 hours, a polymerization reaction started and let to a runaway reaction as a resu lt of heat accumulation. Therefore, the p ressure inc reased, and co mbustible gas leaked out. The gas accumulated in the factory and wa s ignited by a spark from the electric devices t hat were installed outside the dangerous facility zone. Staff members of the manufacturing section had thought at t hat time that a po lymerization reaction would not occur at a low temperature of 27 . However, it appeared that the polymerization reaction started by the delay of the monomer charge to the reactor that resulted from the first accident. When the plant was shutdown, there was st ill about 3800 kg of liquid in the monomer mixing drum.

1. Event

At this plant, AS resin (a co-polymer resin of acrylonitri le and styrene) and AB S resin (a t hree-component system co-poly mer resin of styren e, butadien e and acrylonitrile) were ma nufactured, and th ere were fiv e r eactors for AS r esin polymerization. On the day of the first explosion, two reactors named C and G we re being used for polymerization.

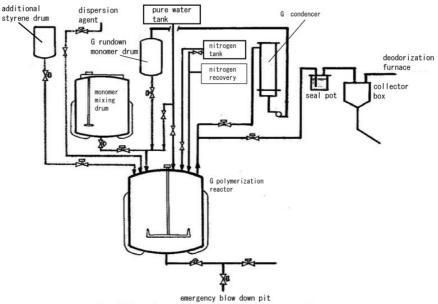


Fig.1 Flow sheet of G polymerization reaction system

The 400V power supply of the polymerization section failed at around midnight. The agitators and pumps for cooling water of the C and G polymerization reactors stopped, so cooling of the reactors stopped. In order to continue cooling, lukewarm supply water was switched to cold water manually. One ton of cold water was a dded to each reactor to cool them. Some time after, the polymerization reaction in the two reactors became a runaway reaction, and white smoky gas spouted from the manhole of the C reactor. The alarm of the d eodorizing furnace rang, and the safet y valve of the furna ce automatically operated, redirecting the gas directly to the stack for combustion tail gas bypassing the furnace. At that time, the concentration of the combustible gas at the furnace inlet was 35% of the lower explosion limit, and the temperature in the furnace exceeded 830 . The fir st exp losion occur red in the exha ust gas d uct, and d amage occurred only in the furnace system.

The reason why a large amount of gas flowed i nto the furn ace system is explained below. The liquid in the C and G reactors separated into two la yers, a polymer layer and a monomer layer, because agitation in the reactors stopped. Furthermore, since the heat of reaction was not being removed, a rapid polymerization reaction occurred, and the liquid t emperature reached the boiling point as a result of heat generated by t he exothermic reaction. The remained monomer evaporated, and a combustible gas w as formed. The combustible gas flowed from the pressure regulating valve via the vent gas collector t o the furn ace system. The furnace system diagram is shown in Fig.2.

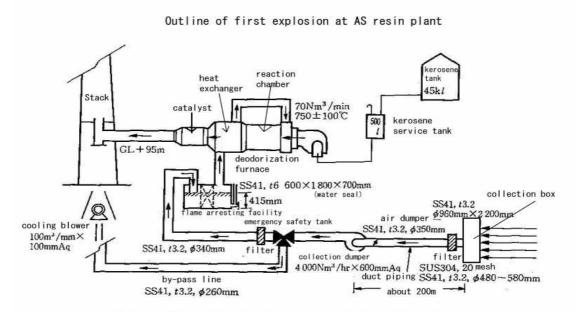


Fig. 2 Flow sheet of the deodorization furnace

The furnace had the following instrumentation system installed for safety: when the combustible gas composition exceeds 50% of the lower explosion limit, or the furna ce temperature is over 830 , the gas is redirected through bypass piping and led to the stack which discharges the gas after it is burned. I n this ac cident case, the instrumentation system worked as designed.

After the fir st explosion, a stop order of the facilities was given by the fire fighting authorities. Therefore, the employees of the factory carried out only the necessary protection work such as drawing off the remaining material in the reactors in order to stop the plant in safe. The next day, thirteen managers of the factory had a preliminary meeting for the accident investigation committee at the same time as the shutdow n procedure was being executed. In the evening, gas began leaking from the monomer mixing drum of the C series. An operator who found the leakage tried to enter the building in order to confirm the sit uation, but he could not enter the building because the leak had increased. Some of the operators left the site to take refuge. One of them informed the managers at the meeting of the leak. All the members attending the meeting rushed to the site. The second hug e explosion occurred when they were preparing to cool the mixing drum by spraying water on it with fireplugs.

2. Course

2.1. Course of the first explosion

At around 23:52 on August 19th, abnormal behavior of the agitators of the polymerization reactors was n otified, and an operator in the electric d evice r oom checked the causes. While he was checking, an electromagnetic switch burned out. He cut the pow er supply after he informed the in cident to the manufacturing section. At that moment, although two reactors were operating, the agitators and the warm water circulation pumps for removing the reaction heat through thermal jackets stopped. The cooling water was switched to cold water manually in order to continue the cooling.

At around 00:10 on August 20th, gas began to leak from the packing part of the manhole of the C reactor. The alarm of the furnace rang at 00:15. The bypass valve of the furnace opened, and the combustible gas before combustion was directly discharged into the stack for burnt tail gas. The temperature inside the furnace exceeded 830 at that time.

At around 00:20, the gas detector in the building operated. At around 00:25, one operator heard the sound of the first exp losion. The operators tried to extinguish the fire with the outdoor fireplugs and reported the explosion to the related parties.

At 00:28, the public fire brigade turned out, and the fire was extinguished at 00:31.

2.2. Course of the second explosion

As the fire extinguishment was reported, from around 00:30 on August 20th, the factory members start ed to check the factory. The check and confirmation work continued during a whole day. The check work was executed mainly around the two reactors. The managing staff members were busy grasping the situation, explaining the situation to the fire fighters and to the police, and reporting the situation to the headquarters.

At 13:00 on August 21st, the preliminary meeting was started by the factory staff members for preparing for the accident cause investigation committee at headquarters. This meeting continued until after 17:00.

At 17:12, a whistling sound was heard fr om the room where the reactors were installed. When an operator looked into the room to check, he found a white gas coming out from the G reactor. Another operator contacted the managers at the meeting. All of the members of the me eting hurried to the site. The white gas flowed from the room towards the north-sid e center road. At around 17:25, the members of the me eting gathered ar ound two firep lugs, and while preparing to spray the site with water , a huge explosion occurred.

3. Cause

3.1. Cause of the first explosion

Stopping of the agitat or by a power failu re caused a runaway reaction in the two reactors and the m onomers (styrene, ac rylonitrile) in the react ors evaporated. The evaporated gas was int roduced into the furnace system of the vent system where the capacity was assumed to be designed for the normal operation, and the furnace was bypassed, since the temperature in the furnace became higher than the furnace design temperature. The monomer vapor was ignited by some ignition sauce, and it exploded in the duct of the furnace syst em. Therefore, a pow er failure and the subseq uent runaway reaction are the direct causes of the explosion.

The occur rence of the power failure may be a cause of the accident, but power failures can occur anywhere. The problem is why a runaway reaction occurred after the power failure and why t he explosion occurred after the ru naway reaction. The plant was not designed for safety in the event of a power failure and the operation manual did no t co ntain appro priate o peration pr ocedures for a p ower failure. Two items mentioned above must be true causes.

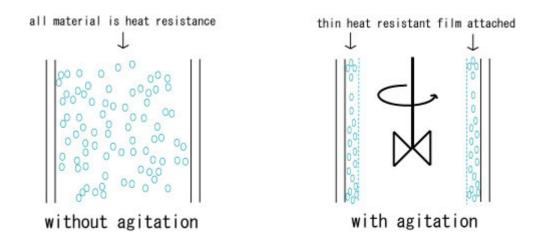


Fig. 3 Effect of an agitation -1 heat transfer

To begin with, the effect of the ag itation stop is d iscussed. The p roblem can b e considered from two aspects. The first is heat t ransfer. When agitation stops in a big vessel with a diameter of 2 met ers, it is not possible to cool the liquid in the v essel. Agitation makes a lami nar film on the heat transfer surface thinner, decreasing heat transfer resistance, equalizing the temperature of the content liquid, and thus cooling is carried out. Considering the size of the agitation drum, which is on an indust rial scale, it is apparent that effective heat tran sfer is not possible, if the agitation stops. Furthermore, the p olymer in the react or is p revented from sep arating from the monomer by agitation, causing the reaction to advance at a moderate rate. The polymer, which is solid and has a high density, separates from the low density monomer, if the agitation stops. The monomer layer with no polymer has high reaction potential. As agitation stopped, heat coul d not be removed from the monomer layer, and a hot spot was easily formed. The polymerization in the monomer layer advanced, and a runaway reaction occurred. A s a result of the te mperature ri se, it se ems to have been unavoidable that the monomer evaporated, its pressure rose, and the vent gas of the monomer increased.

The next aspect is the small capacity of the furnace. As only two out of five resinn reactors were in operation at the time of the power failure, a bypass was inevitable. The combustible gas-air mixture that was redirected to the stack did not burn for that reason, and the explosion occurred as a result. The exact reason why the combustible gas-air mixture was formed is unknown, but there seemed to be some problems in the deodorization system of the vent gas. It can be supposed that there were some problems in the vent gas system that might cause an explosion under the conditions resulting from a power failure.

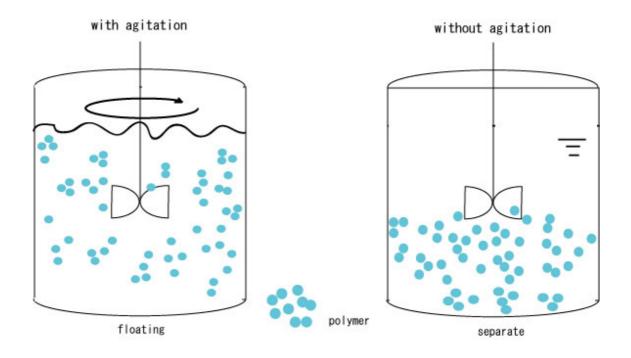
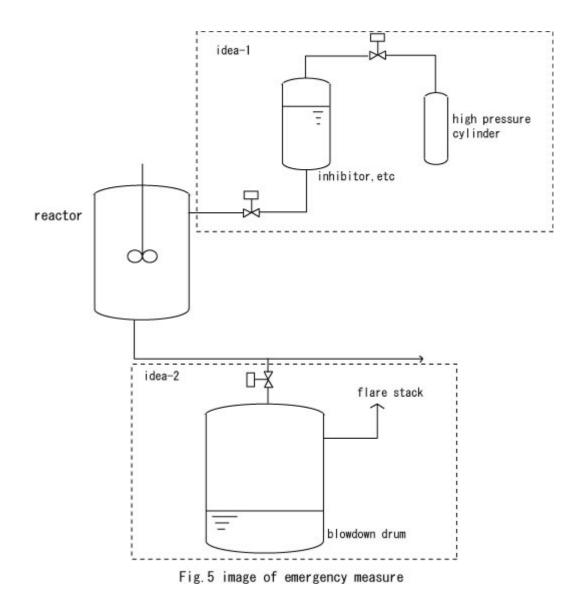


Fig. 4 Effect of an agitation -2 mixing

At present, more safety mechanisms for a power failure can be designed, as shown in Fig.5. For instance, a large blowdown drum with diluents or coolants can be installed d for r eceiving the reactor c ontents or an inhibitor drum can be installed with a high-pressure inert gas cylinder to add the polymerization inhibitor to the react or. Fig.1 shows that p iping to the emergency discharge pit is mounted from the draw-off nozzle at the react or bottom. Although the contents of the discharge pit are unknown, the piping seems to be emergency piping through which the slurry and the liquid in the reactor could be discharged to a safety vessel when a runaway react ion occurred or predicted to occur. If this case, it is a question why the piping was not used.



3.2. Cause of the second explosion

The cause of the se cond exp losion is though t to be as follows. Since the raw material that had been prepared before the first exp losion was l eff for hours in the monomer mixing drum, a polymerization reaction was caused in the drum. Therefore, the temperature rose, and a gas le akage was c aused by the associated pressure rise. The p repared raw material was a mixture of about 3.8 tons of highly reactive acrylonitrile and styrene with initiator added.

Originally, the prepared raw material would have been transferred to the reactor one hour after preparation and it would have reacted by controlling the temperature in the batch. However, since the raw material was left in the monomer mixing drum for 42 hours because of the first explosion, a runaway reaction occurred. The temperature after the preparation was 27 , and it may have been thought that no reaction would occur at that low temperature. Furthermore, from the equipment aspect, the prepared raw material in the monom er mixing drum had to be transferred and reacted in the reactor.

Therefore, the true causes of the accident appeared to be one of the following three; insufficient study of safe storage of the prepared raw material on the R&D stage, insufficient process design for the prepared raw material, and the fact that all the factory members did not pay attention to indispensable material for the sake of urgent countermeasures to the explosion.

The h uman damage resulting from the se cond exp losion was huge . A ll of th e members at the meeting went to the site to gether without sufficient confirmation of safety. This action appears to be one of the causes that increased the human damage. It is necessary to construct a system that gives sufficient information so that the director can make an accurate judgment in the event of an emergency.

4. Process of cause elucidation

The cause of the first explosion can be easily understood from a series of events after a power failure, operation records and the testimonies of the parties concerned. Most of the official a ccident investigation report was concerned with the second explosion and there was no description of the elucidation of the cause of the first explosion.

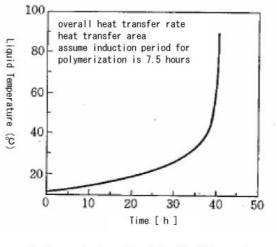


Fig. 6 experiment result of the liquid temeprature increasing in the monomer mixing drum

Regarding the second explosion, the blast center was d etermined almost perfectly from t estimony of with ess and on-site stud y. The so urce of the lea ked vap or was

confirmed according t o the order b elow; 1) To specify the vessel where the sufficient quantity of the gas remained, 2) T o clarify the reason why the gas leaked from the vessel. The monomer mixing drum and the reactor were assumed the vessel where the gas might leak. The quantity of monomers that remained in the reactor was too small for the size of the second explosion. In the monomer mixing drum, there was about 3.8 tons of raw material monomers which was a sufficient quantity to cause the explosion.

After careful experiments, it was confirmed that the monomers in the mixing drum had begun to react at a relatively low temperature and thus the gas leakage occurred. Since the s ize and for ce of the explosion c ould be explained if leakage from the monomer mixing drum was assumed, it was concluded that the gas leakage was caused by a rise in pressure due to a polymerization reaction that had occurred during the long hours of storage in the drum.

5. Immediate action

In the first explosion, four employees of the resin factory carried out the emergency notification by an alarm and an office phone. In addition, they used outdoor fireplugs to extinguish the fire. One fire engine of the factory turned out, and careful preparations were made in front of the resin factory.

At the time of the s econd explosion, the company members were spraying water from one firep lug on the site and p reparing to use oth er firep lugs. The f ollowing activities were carried out after the explosion: notice to the fire fight ing authorities, rescue of the victims, and emergency rescue requests to the fire fighting authorities. After the municipal fire fighting team a rrived, the company's fire fighting team executed rescue activities and continued to spray water on the site using outdoor fireplugs under the supervision of the municipal fire fighting team. After extinguishing the fire, they continued to cool the tank yard by spraying water on it for three days.

6. Countermeasure

The future countermeasures, which cover as much as 14 pages, are described in the accident investigation report. I n order to assure countermeasures for complete safety, man y items ar e d escribed from man y aspects such as management of environmental problems in the neighboring regions, a system for long-distance security and fire p revention, establishment of organizations for d isaster prevention, education and so on.

Here, the basic stance of the technical aspect is described.

1. Safety design of the plant: installation of adequate safety systems in the plant

is important to p revent the oc currence of large -scale disasters by mini mizing the effect of a s mall accident, failure or damage in the plant. Base d on this viewpoint, redundancy, automatization and mechanization of the control system should be considered. Also, in terlocks and depressurizing devices should be prepared for emergent situations. At the plant where the accident occurred, there seemed to be a lack of study of the cap acity of the furna ce and of consideration of countermeasures when the furnace is by-passed.

- 2. Improvement of the f acilities: it is natural to sufficiently consid er the structure and arrangement of the plant. In particular , the plant should be equipped with an early detection method devices and safe shutdown system for emergencies. In addition, if the supply of the utilities fails, prolonged operation of the plant is not possible. The st eady supply of the utilities must be assured. Utilities include el ectric power, steam, and cooling water, which are necessary for plant operation. For example, isolation and duplication of the power supply, and spare diesel driven pumps for cooling water should be considered.
- 3. Related to chemical reactions: the characteristics of the reactions in the process must be sufficiently understood, and facilities and handling methods should be established according to the charact eristics. At the plant where the accident occurred, it would have been effective to have an agitation method of injecting nitrogen gas to maintain the cooling e ffect when agitation stops and t o have blowdown facilities.
- 4. Thoroughness of op eration stand ards and education: ev en the best safety design and the best construction of the p lant are us eless if they are n ot reflected in operations. It is important to prepare operation standards based on the c onsideration of t he characteristics, d angers of the reactions and the materials, the characteristics of the plant, and to educate the operators based on the operation standards.

7. Knowledge

- In abnormal situations, unusual phenomena may occur that cannot be imagined under n ormal operation cond itions. It is important to prepare faci lities and operation methods considering for utility failures because utilities are the lifeline of the plant.
- Chemicals may have to be retained for an unexpectedly long period of time or at unpredicted temp eratures. It is n ecessary to carry out pr ior examinations of these cases.

- 3) In the case of an emergency, it is d angerous for all of t he members to take th e same action and/or the same way of thinking. It is necessary to organize a system for allotting the rol es of investigation, total management, and so on to each member.
- 4) Process design and operational control based on sufficient consideration of what can happen when agitation stops are n ecessary. It is also n ecessary to consider the way of education in an emergency.

8. Influence of failure

All of the human d amage caused by the second explosion was the d eaths of six persons and the injured of 207 persons. Among the injured the number of inhabitants of the neighboring area was 178.

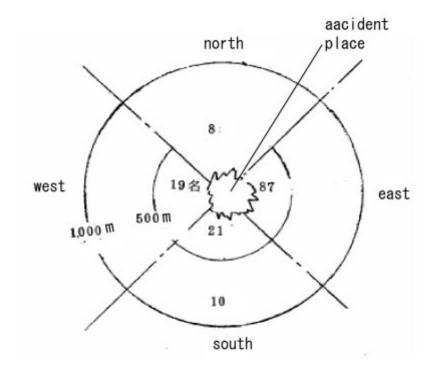


Fig.7 distribution of human damage

The physical damage was as follows; 1733 buildings of 2812 households in the area within the average radius of 1400m were da maged. As the factory in the densely populated area, considerable damage was caused to the neighboring area.

In the factory, many facilities were burned and were damaged by a blast.

The direct monetary damage has been calculated to be about one billion yen. However, the total damage including compensation, indemnities, restoration expenses and the cost of not operating the plant must be far more.

9. On the side

An exp losion of a ch emical p lant in an ov erpopulated region is un expectedly common. A benzoyl peroxide explosion in It abashi Ward of Tokyo, and a hydroxylamine explosion along the national road route 17 in Gunma Prefecture are the examples. These cases are also included in "Selected 100 accidents". These accidents resulted in catastrophic damage, a nd made an excessively strong impact on s ociety. Sometimes, isolation of the factory from the overpopulated region may be only o ne method for avoiding disastrous damage caused by an accident that occu rred at a chemical factory. Furthermore, this accident was caused by a problem related to agit ation. Stopping or restarting a gitation is one of the most important situation changes at a plant. One example of an accident that was caused by stopping of agitation is "Fire during Ethylidenenorbornene Manufacturing" which occurred at a factory in Kawasaki and is included in "Selected 100 Accidents". There are also some examples of accidents that occurred du ring restart of agitation in syst ems such as a reaction of concentrat ed sulfuric acid and toluene. What w ill happen when the b asic conditions are changed such as in these examples is a basic p roblem at chemical plants, and these examples must be learned as a basis of safety engineering.

References

- Yoichi Uehara, "Outline of the AS resin plant explosion. Fire and explosion examples",
 J. Japan Soc. for Safety Engineering, 41, 97-111 (2002)
- The fire fighting union in Sakai City & Takaishi City, "Accident investigation report of explosion and fire at the r esin plant in Sakai factory ,Da icel C hemical Industries Ltd." (1983)
- Ikuo Fukuyama, "Explosion by the runawa y reaction", SE series, "Learn fr om accidents" pp. 20-23 Safety Engineering (1987)